

Math 2250-1

Wed 12/7

9.3-9.4 cont'd

- finish the undamped rigid rod pendulum analysis, pages 2-5 Tuesday's notes.

Here are details we worked out yesterday:

$$\theta'' + \frac{g}{L} \sin \theta = 0$$

$$\downarrow \begin{matrix} x = \theta(t) \\ y = \theta'(t) \end{matrix}$$

$$x' = y$$

$$y' = -\frac{g}{L} \sin x$$

equil. solns  $\begin{matrix} y=0 \\ \sin x=0 \end{matrix} \Rightarrow (n\pi, 0) \quad n \in \mathbb{Z}$ .

$$J(x, y) = \begin{bmatrix} 0 & 1 \\ -\frac{g}{L} \cos x & 0 \end{bmatrix}$$

if  $x = n\pi$   
n even,  $\cos x = +1$

if  $x = n\pi$ , n odd,  
 $\cos x = -1$

$$J = \begin{bmatrix} 0 & 1 \\ -\frac{g}{L} & 0 \end{bmatrix}$$

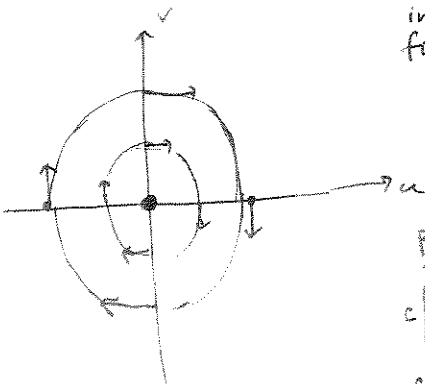
$$\begin{bmatrix} u' \\ v' \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{L} & 0 \end{bmatrix} \begin{bmatrix} u \\ v \end{bmatrix}$$

$$|J - \lambda I| = \lambda^2 + \frac{g}{L} = 0$$

$$\lambda = \pm i \sqrt{\frac{g}{L}}$$

$$= \pm i \omega_0$$

stable center for linearized problem, indeterminate for non-linear



pt.	tang vector
$c \begin{bmatrix} 1 \\ 0 \end{bmatrix}$	$c \begin{bmatrix} 0 \\ -\frac{g}{L} \end{bmatrix}$
$c \begin{bmatrix} 0 \\ 1 \end{bmatrix}$	$c \begin{bmatrix} 1 \\ 0 \end{bmatrix}$

$$J = \begin{bmatrix} 0 & 1 \\ \frac{g}{L} & 0 \end{bmatrix}$$

$$\begin{bmatrix} u' \\ v' \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ \frac{g}{L} & 0 \end{bmatrix} \begin{bmatrix} u \\ v \end{bmatrix}$$

$$|J - \lambda I| = \lambda^2 - \frac{g}{L} = 0$$

$$\lambda = \pm \sqrt{\frac{g}{L}}$$

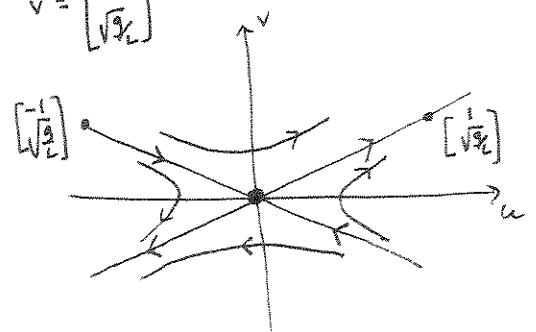
Saddle for linearized & non-linear system

$$\lambda = \sqrt{\frac{g}{L}}$$

$$\lambda = -\sqrt{\frac{g}{L}}$$

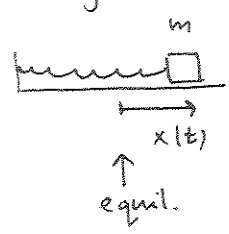
$$\vec{v} = \begin{bmatrix} 1 \\ \sqrt{\frac{g}{L}} \end{bmatrix}$$

$$\vec{v} = \begin{bmatrix} -1 \\ \sqrt{\frac{g}{L}} \end{bmatrix}$$



• After recalling page 1, complete pages 3-5 Tuesday's notes

Then consider a non-linear modification of the mass-spring configuration



$$m x''(t) = F(x)$$

$$m x''(t) = -kx + \alpha x^2 + \beta x^3 + \dots$$

linear model:  $m x''(t) = -kx$   
assumes perfect Hookeian spring.

improvements: consider more terms in Taylor series, could model a variety of situations.

→ if force is an odd function,  $F(-x) = -F(x)$ , then only odd powers appear in Taylor series, and a good model might be

$$m x'' = -kx + \beta x^3$$

$\beta < 0$  "hard spring" (resists large deviations  $x$ )  
 $\beta > 0$  "soft spring"

→ force might not be odd, in which case

$$m x'' = -kx + \alpha x^2$$

might be a good model (resists  $x < 0$  more than  $x > 0$ )

First order system for  $m x''(t) = F(x)$

$$\begin{cases} x' = y \\ y' = \frac{1}{m} F(x) \end{cases}$$

so  $x(t)$  = position  
 $y(t)$  = velocity.

Because the Force does not depend on velocity these systems always have a conserved total energy function. It can be recovered either using the concept of work from Calculus/Physics, or with the  $\frac{dy}{dx} = \frac{dy/dt}{dx/dt}$

separable DE's trick.

$$TE = KE + PE$$

$$= \frac{1}{2} m y^2 + \int_0^x -F(s) ds$$

$$\frac{d}{dt} (TE) = m y y' - F(x) x'(t)$$

$$= m x' \left( \frac{1}{m} F \right) - F x' = 0$$

$$\frac{dy}{dx} = \frac{\frac{1}{m} F(x)}{y}$$

$$m y dy = F(x) dx$$

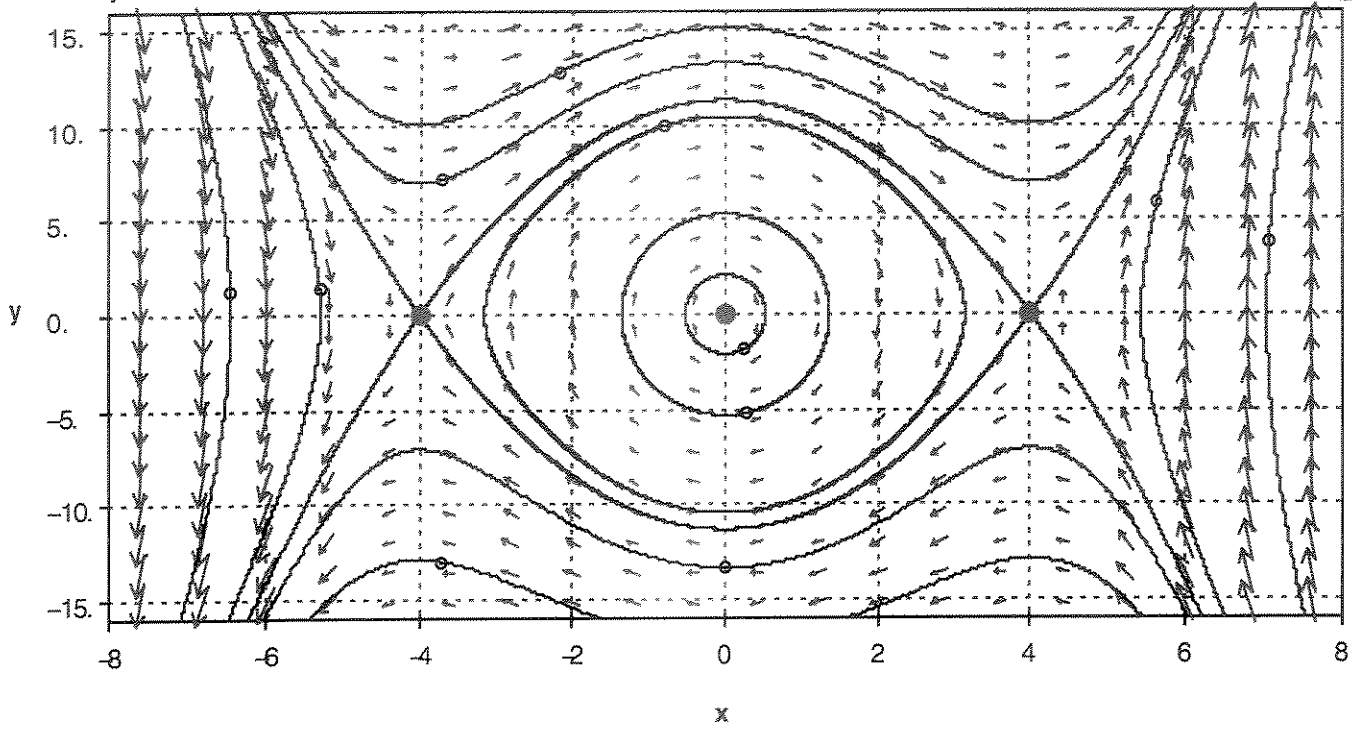
$$\frac{1}{2} m y^2 = \int F(x) dx + C$$

Exercise 1 : Consider the "soft spring" problem

$$x''(t) = -16x + x^3$$

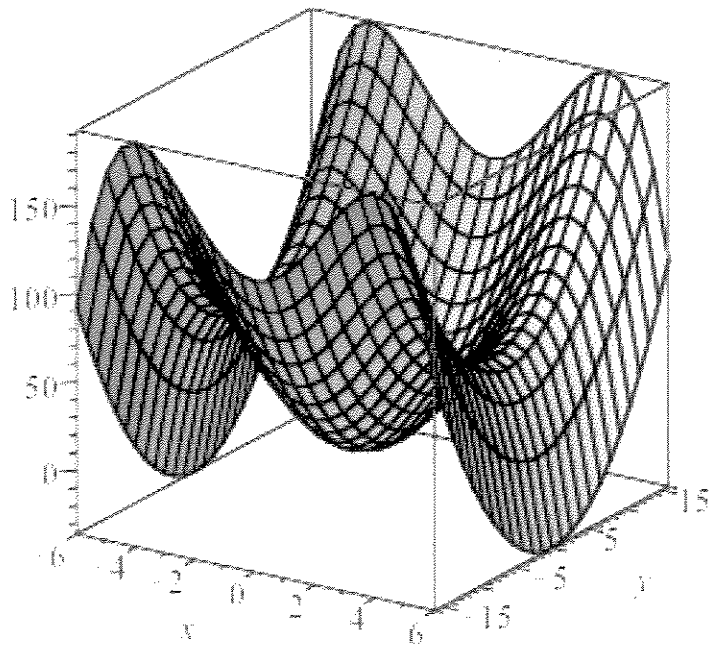
- a) Convert this to an equivalent 1<sup>st</sup> order system
- b) Find the equilibrium solutions
- c) Verify that the linearizations are consistent with the phase portrait, at the equilibria.
- d) What is the total (conserved) energy in this problem?

$$\begin{aligned} x' &= y \\ y' &= -16x + x^3 \end{aligned}$$



soft spring total energy function

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> with(plots):
> plot3d( (y^2)/2 + 8*x^2 - x^4/4, x=-6..6, y=-16..16, axes = boxed );
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